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**Neutron Production from (α ,n) Reactions and
Spontaneous Fission in ThO_2 , UO_2 , and
 $(\text{U,Pu})\text{O}_2$ Fuels**

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Neutron Production from (α, n) Reactions and Spontaneous Fission in ThO_2 , UO_2 , and $(\text{U, Pu})\text{O}_2$ Fuels

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NEUTRON PRODUCTION FROM (α ,n) REACTIONS AND SPONTANEOUS FISSION
IN ThO₂, UO₂, AND (U,Pu)O₂ FUELS

by

R. T. Perry and W. B. Wilson

ABSTRACT

Available alpha-particle stopping cross-section and ^{17,18}O(α ,n) cross-section data were adjusted, fitted, and used in calculating the thick-target neutron production function for alpha particles below 10 MeV in oxide fuels. The spent UO₂ function produced was folded with actinide decay spectra to determine (α ,n) neutron production by each of 89 actinides. Spontaneous-fission (SF) neutron production for 40 actinides was calculated as the product of $\bar{\nu}$ (SF) and SF branching-fraction values accumulated or estimated from available data. These contributions and total neutron production in spent UO₂ fuel are tabulated and, when combined with any calculated inventory, describe the spent UO₂ neutron source. All data are tabulated and methodology is described to permit easy extension to specialized problems.

I. INTRODUCTION

Neutron sources are present in reactor fuel from the spontaneous-fission (SF) decay of actinide nuclides and from the interaction of their decay alpha particles with low- and medium-Z nuclides in (α ,n) reactions. The (α ,n) source in oxide fuels is dominated by reactions with ¹⁷O and ¹⁸O, which are present in NATO in 0.038 and 0.204 atom percent abundancies, respectively.

The probability of neutron production by an alpha particle emitted at energy E_α in the fuel is given by the thick-target neutron production function $P(E_\alpha)$, which we have evaluated for four fuel compositions--clean ThO₂ thermal

reactor fuel, clean and spent UO_2 thermal reactor fuel, and clean $(U,Pu)O_2$ fast reactor fuel. The (α,n) neutron production function has been evaluated at the Hanford Engineering Development Laboratory (HEDL) by Ombrellaro and Johnson for alpha particles in FFTF fuel;¹ however, $P(E_\alpha)$ has not been calculated for the fuels of interest here, and the change in $P(E_\alpha)$ with exposure has not been evaluated. We have employed the methodology and data used in the HEDL work¹ with minor exceptions in data and energy range of calculation.

The equations describing (α,n) and SF neutron production and the data quantities used in the calculations are given in Sec. II. The available data sources and adjustments made to the data are described in Sec. III. Details of the (α,n) calculations are briefly discussed in Sec. IV. Resulting (α,n) , SF, and total neutron production values are given in Sec. V for each of a variety of actinide nuclides produced in reactor fuels.

Selected results of these calculations have been reported previously.²⁻⁵

II. THEORY

The slowing and stopping of alpha particles in a material are described by the material's alpha-particle stopping power,

$$SP(E) = - \frac{dE}{dx} , \quad (1)$$

which gives the energy-dependent energy loss of alpha particles of energy E per unit path length x .⁶ The energy loss of an alpha particle of initial energy E_α in traveling a distance X can be determined from the stopping power as

$$\Delta E = E_\alpha - E'_\alpha = \int_0^X \left(- \frac{dE}{dx} \right) dx . \quad (2)$$

Similarly, the distance traveled in slowing from E_α to E'_α is

$$X = \int_{E'_\alpha}^{E_\alpha} \frac{1}{\left(\frac{dE}{dx} \right)} dE = \int_{E'_\alpha}^{E_\alpha} \frac{1}{\left(- \frac{dE}{dx} \right)} dE . \quad (3)$$

Neutrons may be produced within the material by (α, n) reactions with nuclide i , which has atom density N_i and microscopic (α, n) cross section $\sigma_i(E)$. The probability of (α, n) interaction with nuclide i by an alpha particle of energy E traveling from x to $x + dx$ is

$$N_i \sigma_i(E) dx = \frac{N_i \sigma_i(E) dE}{\left(\frac{dE}{dx}\right)} \quad (4)$$

The probability of (α, n) interaction with nuclide i by an alpha particle in lieu of slowing from E_α to E'_α is then

$$p_i(E_\alpha, E'_\alpha) = \int_{E'_\alpha}^{E_\alpha} \frac{N_i \sigma_i(E) dE}{\left(\frac{dE}{dx}\right)} = \int_{E'_\alpha}^{E_\alpha} \frac{N_i \sigma_i(E) dE}{\left(-\frac{dE}{dx}\right)} \quad (5)$$

The probability of (α, n) interaction with nuclide i by an alpha particle prior to stopping in the material is given by the thick-target neutron production function

$$P_i(E_\alpha) = \int_0^{E_\alpha} \frac{N_i \sigma_i(E) dE}{\left(-\frac{dE}{dx}\right)} \quad (6)$$

In addition to that of the above definition of Eq. (1), a variety of quantities are referred to as "stopping powers" or often alternately "stopping cross sections." These include (typically without explicit regard to sign) the quantities $\frac{dE}{dx} = \frac{dE}{d(\rho x)} = \frac{dE}{\rho dx}$, $\frac{dE}{Z^2 dx}$, $\rho \frac{dE}{dx}$, and $\frac{dE}{N dx}$. Here x is material thickness (mg/cm^2), Z is atomic number, ρ is material density (g/cm^3), and N is the total atom density of the material (atoms/cm^3). The last quantity is also called the stopping cross section,

$$\epsilon(E) = -\frac{1}{N} \frac{dE}{dx} \quad (7)$$

a notation adopted here. Equations above defining p_i and P_i may now be written in terms of ϵ as

$$P_i(E_\alpha, E'_\alpha) = \frac{N_i}{N} \int_{E'_\alpha}^{E_\alpha} \frac{\sigma_i(E)}{\epsilon(E)} dE \quad (8)$$

and

$$P_i(E_\alpha) = \frac{N_i}{N} \int_0^{E_\alpha} \frac{\sigma_i(E)}{\epsilon(E)} dE \quad (9)$$

Note that p_i and P_i are related by

$$p_i(E_\alpha, E'_\alpha) = P_i(E_\alpha) - P_i(E'_\alpha) \quad (10)$$

The stopping cross section $\epsilon(E)$ of a material composed of J elemental constituents may be calculated using the Bragg-Kleeman¹⁰ relationship, which may be written as

$$\epsilon(E) \approx \frac{1}{N} \sum_{j=1}^J N_j \epsilon_j(E) \quad (11)$$

where

$$N = \sum_{j=1}^J N_j \quad (12)$$

The accuracy of the approximation of Eq. (11) will be discussed in Sec. III.

A fraction of the decays of nuclide k within the material may be by alpha-particle emission. This fraction F_k^α of alpha decays may occur with the emission of one of L possible alpha-particle energies. The intensity $f_{k\ell}^\alpha$ is the fraction of all decays of nuclide k resulting in an alpha particle of energy $E_{k\ell}$, and

$$F_k^\alpha = \sum_{\ell=1}^L f_{k\ell}^\alpha \quad (13)$$

The fraction of nuclide k decays resulting in (α, n) neutron production in a thick-target material containing I nuclides with (α, n) cross sections is thus

$$R_k(\alpha, n) = \sum_{\ell=1}^L f_{k\ell}^{\alpha} \sum_{i=1}^I P_i(E_{k\ell}) \quad . \quad (14)$$

The SF of an actinide nuclide k is accompanied by the emission of an average $\bar{\nu}_k$ (SF) neutrons. The SF activity A_k^{SF} of nuclide k , having atom density N_k , is

$$A_k^{SF} = \lambda_k^{SF} N_k \quad . \quad (15)$$

Here, λ_k^{SF} is the SF decay constant defined by

$$\lambda_k^{SF} = \ln 2 / T_{1/2}^k(SF) \quad , \quad (16)$$

where $T_{1/2}^k(SF)$ is the SF half-life of nuclide k . SF is typically only one of M modes of decay; the total activity due to nuclide k is

$$A_k = \lambda_k N_k = \sum_{m=1}^M A_k^m \quad , \quad (17)$$

where λ_k is the total decay constant of nuclide k ,

$$\lambda_k = \sum_{m=1}^M \lambda_k^m = \ln 2 / T_{1/2}^k \quad , \quad (18)$$

and $T_{1/2}^k$ is the total half-life of nuclide k . The fraction of nuclide k decays by SF is given by the SF branching fraction

$$F_k^{SF} = A_k^{SF} / A_k = \lambda_k^{SF} / \lambda_k = T_{1/2}^k / T_{1/2}^k(SF) \quad . \quad (19)$$

The average number of SF neutrons emitted per decay (by any mode) of nuclide k is then

$$R_k(\text{SF}) = F_k^{\text{SF}} \bar{\nu}_k(\text{SF}) \quad . \quad (20)$$

The total number of neutrons, on the average, emitted due to (α, n) reactions and SF is

$$R_k = R_k(\alpha, n) + R_k(\text{SF}) \quad . \quad (21)$$

The total neutron source S from (α, n) reactions and SF within a material containing K pertinent radionuclides is then

$$S = \sum_{k=1}^K \lambda_k N_k R_k \quad . \quad (22)$$

The evaluation of the quantities $R_k(\alpha, n)$, $R_k(\text{SF})$, and R_k for a number of actinide nuclides is described in the following sections.

III. DATA

The data quantities required to compute the neutron production fractions $R_k(\alpha, n)$ and $R_k(\text{SF})$ for each of the four fuels of interest include the following.

- For each major elemental constituent j of the material: N_j , the atom density; and $\epsilon_j(E)$, the alpha-particle stopping cross section.
- For each nuclide i within the material having an (α, n) cross section: N_i , the atom density; and $\sigma_i(E)$, the microscopic (α, n) cross section.
- For each nuclide k decaying by alpha decay: $f_{k\ell}^\alpha$, the intensity for emission of each L alpha particles; and $E_{k\ell}$, the energy of each of L alpha particles.
- For each nuclide k decaying by SF: F_k^{SF} , the SF branching fraction; and $\bar{\nu}_k(\text{SF})$, the average number of neutrons emitted per SF.

A. Stopping Cross Section $\epsilon(E)$

Densities of each constituent of each fuel type are given in Table I. The fuel composition of UO_2 LWR fuel is given for clean and spent conditions for the evaluation of the effect of exposure-dependent fuel composition on stopping cross section ϵ ; here, $_{41}Nb$ and $_{59}Pr$ represent the low- and high-mass fission products, respectively. Concentrations of $_{93}Np$, $_{95}Am$, and $_{96}Cm$ are given for the spent UO_2 fuel, although the minor contributions to ϵ from these nuclides are included as plutonium. Elements contributing to the material stopping cross sections are thus O, Nb, Pr, Th, U, and Pu.

A bibliography of experimental and theoretical stopping-power references by Anderson¹¹ notes that some 900 papers have been published on the subject of ion energy loss in matter. Anderson, noting the observation by Bichsel¹² that stopping powers measured by different groups often did not agree within stated uncertainties, was unable to resolve discrepancies after careful analysis and cautioned that stopping-power data sources should be selected carefully. We have chosen as the major stopping cross-section data source the comprehensive volume edited by Ziegler,¹³ which gives tabulated alpha stopping cross-section values and functional fits for elements in the range $1 \leq Z \leq 92$.

No values of the alpha-stopping cross section for plutonium were identified, although values for plutonium compounds were found.⁷ Northcliffe and Schilling⁸ have tabulated values of the stopping power $dE/d\chi$ for $Z \leq 92$. They have shown graphically, for each Z including $Z = 94$, the energy-dependent ratio $(dE/d\chi)_Z : (dE/d\chi)_{Al}$. In order to form a stopping cross section for plutonium consistent with the data of Ziegler,¹³ we have used the stopping power ratio of Ref. 8 in the expression

$$\epsilon_{Pu} = \epsilon_u \frac{A_{Pu}}{A_U} \left[(dE/d\chi)_{Pu} : (dE/d\chi)_{Al} \frac{(dE/d\chi)_{Al}}{(dE/d\chi)_U} \right], \quad (23)$$

where all quantities enclosed in brackets [] were taken from Ref. 8. Values used and produced in this calculation are given in Table II.

Fourth-degree polynomial functions of the form

$$\ln \epsilon = C_0 + C_1 \ln E + C_2 \ln^2 E + C_3 \ln^3 E + C_4 \ln^4 E \quad (24)$$

TABLE I
 PROPERTIES OF OXIDE FUELS

	Thermal Reactor Fuels			Fast Reactor Fuel (U,Pu)O ₂ Clean
	UO ₂ Clean	UO ₂ Spent	ThO ₂ Clean	
Fuel Density (g/cm ³)	9.95	9.95	9.17	9.62
Exposure Gwd/t	0	34	0	0
<u>Atom Densities (atoms/b-cm)</u>				
NAT ₈₀	0.04372	0.04372	0.04184	0.04215
¹⁶ O	0.04361	0.04361	0.04174	0.04205
¹⁷ O	1.6614-5	1.6614-5	1.5899-5	1.6017-5
¹⁸ O	8.9189-5	8.9189-5	8.5354-5	8.5986-5
⁴¹ Nb	0	7.893-4	0	0
⁵⁹ Pr	0	7.893-4	0	0
⁹⁰ Th	0	0	0.02025	0
⁹² U	0.02186	0.02085	6.724-4	0.01887
⁹³ Np	0	1.043-5	0	0
⁹⁴ Pu	0	2.037-4	0	0.002634
⁹⁵ Am	0	5.692-6	0	0
⁹⁶ Cm	0	1.131-6	0	0

TABLE II

DATA OF NORTHCLIFFE AND SCHILLING^a AND ZIEGLER^b USED IN
CALCULATING THE ALPHA PARTICLE STOPPING CROSS SECTION OF PLUTONIUM

E_{α} MeV	Stopping Power Ratios and Values from Northcliffe and Schilling				$\epsilon(E)$ Stopping Cross Section	
	$(dE/d\chi)_{Pu}$	$(MeV/mg/cm^2)$		$(dE/d\chi)_{Pu}$	$eV/(10^{15} \text{ atoms/cm}^2)$	
	$(dE/d\chi)_{Al}$	$(dE/d\chi)_{Al}$	$(dE/d\chi)_{U}$	$(dE/d\chi)_{U}$	U(Ziegler)	Pu(Calculated)
0.100	0.150	0.752	0.135	0.837	75.80	63.74
0.320	0.188	1.219	0.243	0.942	139.93	132.48
0.500	0.214	1.317	0.286	0.986	165.64	164.08
0.805	0.235	1.299	0.312	0.978	178.59	175.40
1.281	0.256	1.170	0.307	0.977	166.77	163.72
2.402	0.291	0.904	0.269	0.978	129.15	126.86
4.003	0.322	0.682	0.223	0.982	100.57	99.23
6.404	0.350	0.512	0.183	0.978	78.65	77.29
10.007	0.382	0.379	0.148	0.980	60.67	59.71
16.010	0.418	0.270	0.114	0.991	47.09	46.90
24.016	0.448	0.200	0.090	1.000	37.01	37.18
48.031	0.490	0.118	0.059	0.983	23.64	23.35

^aNorthcliffe and Schilling, Nucl. Data Tables A7, 233 (1970)

^bJ. F. Ziegler, Helium Stopping Powers and Ranges in All Elemental Matter, Vol. 4 of The Stopping and Ranges of Ions In Matter Series (Pergamon Press, New York, 1977).

were fit to each set of tabulated stopping cross-section values, representing the values within 1% at any energy over the range $0.5 \text{ MeV} \leq E_\alpha \leq 10 \text{ MeV}$. These functional stopping cross sections are shown in Fig. 1. Coefficients of the polynomial functions are given in Table III. Stopping cross sections of the oxide fuels were formed from these component stopping cross-section functions using the Bragg-Kleeman relationship of Eq. (11) and component densities given in Table I.

Stopping cross-section values of UO_2 , ThO_2 , and $(\text{U}_{.8}\text{Pu}_{.2})\text{O}_2$ were computed over the range $2 \text{ MeV} \leq E_\alpha \leq 8 \text{ MeV}$ and compared in Table IV with values of ϵ converted from experimentally measured values of dE/dx reported by Nitzki and Matzke.⁷ The measured and calculated values of ϵ agree within 9% over this range, with calculated values generally lower than measured values.

B. (α, n) Cross Sections

The cross sections for the $^{17,18}\text{O}(\alpha, n)$ reactions have been reported over four limited ranges of E_α , although no single measurement extends over the entire range of our interest. Bair and Willard¹⁴ plotted their measured $^{18}\text{O}(\alpha, n)^{21}\text{Ne}$ cross-section values over the range $2.37 \text{ MeV} \leq E_\alpha \leq 5.15 \text{ MeV}$. Bair and Hass¹⁵ extended the range of these data down to 1.14 MeV and plotted the $^{17}\text{O}(\alpha, n)^{20}\text{Ne}$ cross section over the range $1.31 \text{ MeV} \leq E_\alpha \leq 5.31 \text{ MeV}$. Bair and del Campo¹⁶ later plotted the $^{\text{NAT}}\text{O}(\alpha, n)$ cross section over the range $3.1 \text{ MeV} \leq E_\alpha \leq 8 \text{ MeV}$ and, based on their measured $^{\text{NAT}}\text{O}(\alpha, n)$ neutron production by alpha particles in the range $4.62 \text{ MeV} \leq E_\alpha \leq 4.8 \text{ MeV}$, recommended that the $^{17,18}\text{O}(\alpha, n)$ cross sections reported in Refs. 14 and 15 be increased by 35%.

Differential cross sections $d\sigma(E)/d\Omega$ for $^{17,18}\text{O}(\alpha, n)$ reactions were measured at higher energies by Hansen et al.,¹⁷ who fit their measured angular distributions with Legendre polynomial expansions that they integrated to yield total $\sigma(\alpha, n)$ values. These values were plotted for the range $4.3 \text{ MeV} \leq E_\alpha \leq 12.3 \text{ MeV}$, and smooth curves were plotted approximating each set of data.

Except for cross-section values given by Hansen et al.¹⁷ at 9.8, 11.6, and 12.3 MeV, no data were available in other than graphic form--despite the best efforts of Bair,¹⁸ del Campo,¹⁹ and Hansen²⁰ to resurrect their numerical data. Data taken from the $^{17,18}\text{O}(\alpha, n)$ cross-section curves of Refs. 14 and 15 for the earlier HEDL work¹ were supplied to us.²¹ These data were thinned to 744 values of the $^{17}\text{O}(\alpha, n)$ cross section and 687 values of the $^{18}\text{O}(\alpha, n)$ cross section. Fourth-degree polynomial fits were made to data taken from the

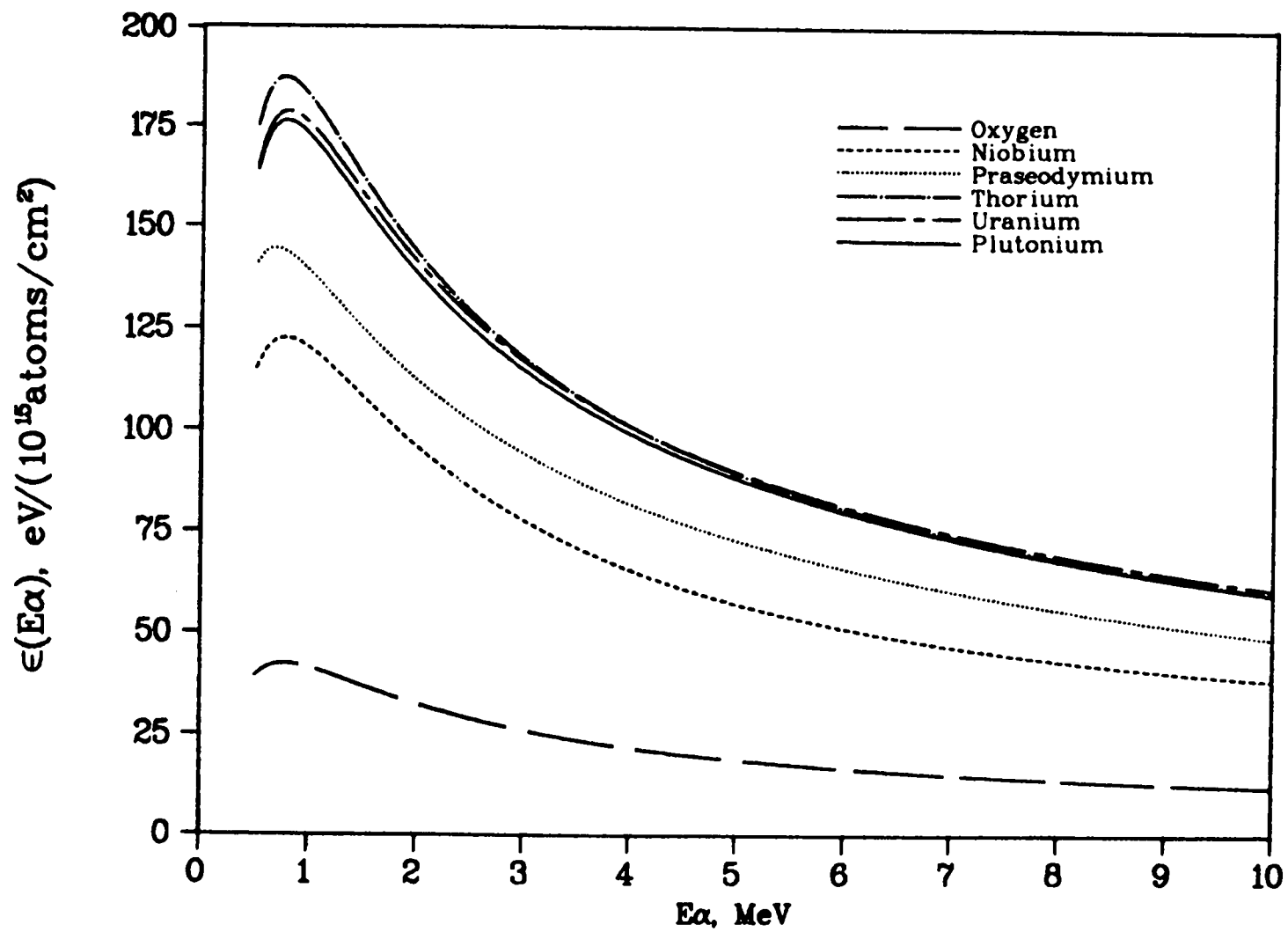


Fig. 1.
Stopping cross sections $\epsilon(E_\alpha)$ of O, Nb, Pr, Th, U, and Pu.

TABLE III

COEFFICIENTS OF POLYNOMIAL FITS TO STOPPING CROSS SECTIONS^a

Element	C ₀	C ₁	C ₂	C ₃	C ₄
O	3.7213	-0.168700	-0.300138	0.0700466	-0.00377296
Ni	4.7872	-0.156294	-0.278932	0.0533399	0.00186590
Pr	4.9321	-0.192312	-0.199561	0.0592391	-0.00940776
Th	5.2027	-0.195369	-0.278809	0.105037	-0.0163945
U	5.1648	-0.161478	-0.279242	0.099232	-0.0146254
Pu	5.1486	-0.171158	-0.272723	0.100975	-0.0160365

^a $\ln \epsilon = C_0 + C_1 \ln E + C_2 \ln^2 E + C_3 \ln^3 E + C_4 \ln^4 E$,
 E is alpha-particle energy in MeV, $0.5 < E \text{ (MeV)} < 10.0$, and
 ϵ is stopping cross section in $\text{eV}/(10^{15} \text{ atoms/cm}^2)$.

TABLE IV

COMPARISON OF CALCULATED AND MEASURED
ALPHA STOPPING CROSS SECTIONS FOR OXIDE FUELS

E MeV	$\epsilon(E)$ for ThO ₂			$\epsilon(E)$ for UO ₂			$\epsilon(E)$ for (U .8Pu .2)O ₂		
	From a	From Table III and Eq. (11)	% Dif	From a	From Table III and Eq. (11)	% Dif	From a	From Table III and Eq. (11)	% Dif
2	68.96	69.40	0.6	71.10	68.73	-3.3	72.17	68.55	-5.0
3	59.38	56.27	-5.2	59.91	55.93	-6.6	60.48	55.84	-7.7
4	52.13	48.67	-6.6	51.76	48.13	-7.0	52.05	48.01	-7.8
5	46.46	42.43	-8.7	45.56	42.53	-6.6	45.69	42.43	-7.1
6	41.91	38.20	-8.9	40.69	38.37	-5.7	40.71	38.27	-6.0
7	38.16	34.87	-8.6	36.76	35.10	-4.5	36.71	35.00	-4.7
8	35.03	32.23	-8.0	33.52	32.50	-3.0	33.42	32.41	-3.0

^a Nitzki and Matzke, Phys. Rev. B8, 1894 (1973).

$^{17,18}\text{O}(\alpha,n)$ cross-section plot of Ref. 16 and to data taken from the $^{17,18}\text{O}(\alpha,n)$ cross-section plots of Ref. 17. These five cross-section descriptions are shown in Fig. 2.

The $^{17,18}\text{O}(\alpha,n)$ cross sections used in the present calculations were composed of the lower energy data of Refs. 14 and 15 increased by 35% as recommended in Ref. 16 and joined with the adjusted higher energy data of Ref. 17. This adjustment, amounting to a 9.2% reduction, was determined by normalizing the integral of the $^{17,18}\text{O}(\alpha,n)$ cross section formed from the functional fits to $^{17,18}\text{O}(\alpha,n)$ cross sections of Ref. 17 to the integral of the $^{17,18}\text{O}(\alpha,n)$ cross section of Ref. 16 over the range $5.15 \text{ MeV} \leq E_\alpha \leq 8 \text{ MeV}$. The resulting adjusted cross sections are shown in Fig. 3. The adjusted $^{17}\text{O}(\alpha,n)$ cross section is given in Table V, and the adjusted $^{18}\text{O}(\alpha,n)$ cross section is given in Table VI; cross sections are defined there by interpolation points at low energies ($\leq 5 \text{ MeV}$) and by polynomial functions at higher energies.

C. Alpha-Decay Data

A total of 144 actinide nuclides produced in reactor fuel have been identified,²² using data of ENDF/B-V and Refs. 23-25. Of these, 89 decay at least partly by alpha decay. Each nuclide has some L different alpha-particle energies with $1 \leq L \leq 26$ for the data collection used. Alpha-particle energies in the data collection fall in the range $3.71 \text{ MeV} \leq E_\alpha \leq 8.78 \text{ MeV}$. TABLE VII lists the alpha-particle energies and intensities for each nuclide.

D. Spontaneous-Fission Data

Of the 144 actinide nuclides identified, 40 decay at least partly by spontaneous fission. Values of $\bar{\nu}_p(\text{SF})$, the major prompt contribution to $\bar{\nu}(\text{SF})$, are given by Manero and Konshin²⁶ for many of these. These values were used in Fig. 4 to estimate values of $\bar{\nu}_p(\text{SF})$ for nuclides without data.

Branching fractions F^{SF} , if not given in a data reference, were constructed from total and SF half-life values $T_{1/2}(\text{SF})$ using Eq. (19). Values of $T_{1/2}(\text{SF})$ given as limiting values were used and quoted without qualification. The values of $\bar{\nu}(\text{SF})$, F^{SF} , and $R(\text{SF})$ for each of the 40 nuclides are given in Table VIII.

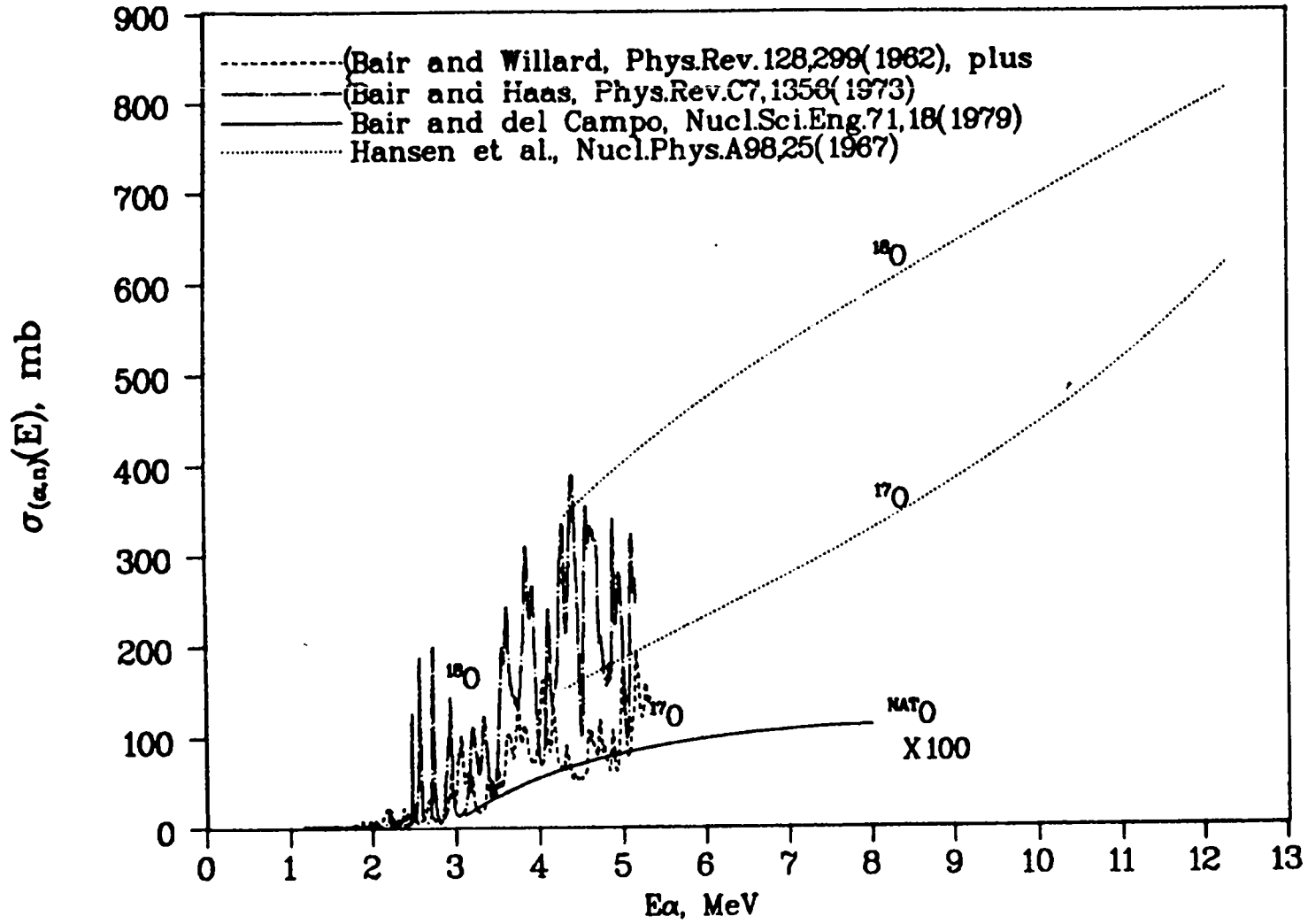


Fig. 2.
 ^{17}O , ^{18}O , and NATO (α,n) cross-section data.

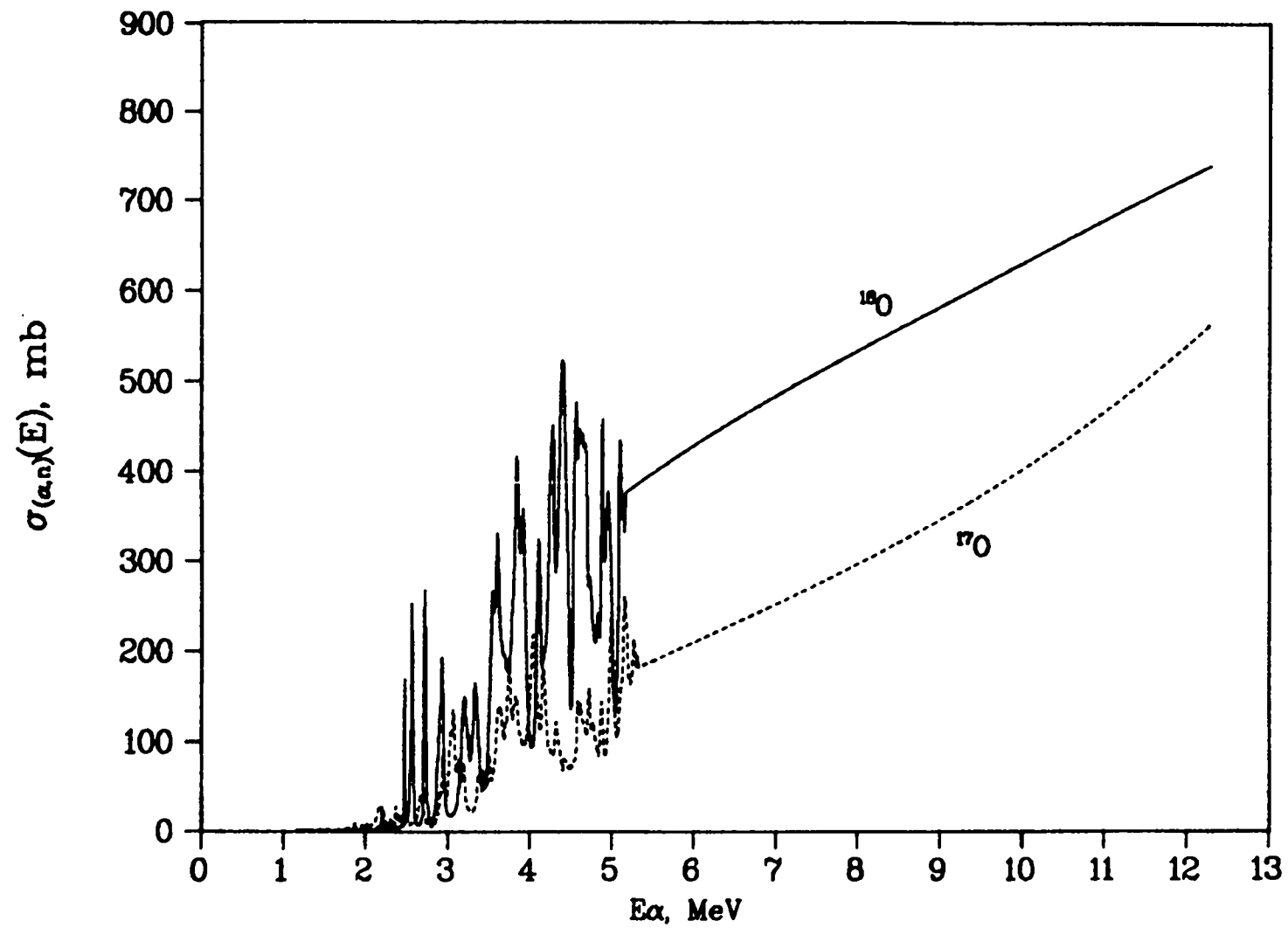


Fig. 3.
 ^{17}O and ^{18}O adjusted (α, n) cross sections.

TABLE VII
ALPHA DECAY SPECTRA OF ACTINIDE NUCLIDES

82-Pb-210 1 ALPHA REF B E,MEV. DK FRACTION 3.7198 1.70000E-08	83-Bi-214 6 ALPHAS REF B E,MEV. DK FRACTION 4.9420 5.25210E-07 5.0234 4.41176E-07 5.1824 1.26090E-06 5.2638 1.21849E-05 5.4508 1.13235E-04 5.5121 8.23529E-05	86-Rn-218 2 ALPHAS REF B E,MEV. DK FRACTION 6.5349 1.30091E-03 7.1331 9.98699E-01	88-Ra-223 12 ALPHAS REF B E,MEV. DK FRACTION 5.2839 1.00000E-03 5.2885 1.30000E-03 5.3399 1.00000E-03 5.3660 1.10000E-03 5.4347 2.30000E-02 5.5025 1.00000E-02 5.5396 9.10000E-02 5.6073 2.40000E-01 5.7161 5.28900E-01 5.7474 9.10000E-02 5.8577 3.20000E-03 5.8718 8.50000E-03	89-Ac-227 8 ALPHAS REF B E,MEV. DK FRACTION 4.7151 4.30252E-05 4.7701 1.94308E-04 4.7967 1.12421E-04 4.8556 5.13527E-04 4.8733 8.46626E-04 4.9008 1.52670E-05 4.9416 5.55164E-03 4.9538 6.52318E-03	90-Th-230 7 ALPHAS REF A E,MEV. DK FRACTION 4.2440 5.00746E-04 4.2780 8.01194E-08 4.3720 1.00144E-05 4.4380 3.00448E-04 4.4800 1.20179E-03 4.6210 2.34344E-01 4.6875 7.64136E-01
83-Bi-210 2 ALPHAS REF B E,MEV. DK FRACTION 4.6479 7.80000E-07 4.6861 5.20000E-07	84-Po-214 2 ALPHAS REF B E,MEV. DK FRACTION 6.9025 1.00000E-04 7.6873 9.99900E-01	85-At-219 1 ALPHA REF B E,MEV. DK FRACTION 6.2733 9.70000E-01	86-Rn-219 4 ALPHAS REF B E,MEV. DK FRACTION 6.4250 7.49101E-02 6.5310 1.19856E-03 6.5532 1.14862E-01 6.8194 8.09029E-01	89-Ac-227 8 ALPHAS REF B E,MEV. DK FRACTION 4.7151 4.30252E-05 4.7701 1.94308E-04 4.7967 1.12421E-04 4.8556 5.13527E-04 4.8733 8.46626E-04 4.9008 1.52670E-05 4.9416 5.55164E-03 4.9538 6.52318E-03	91-Pa-230 18 ALPHAS REF B E,MEV. DK FRACTION 4.7653 6.40446E-08 4.7987 9.60672E-09 4.9343 1.28090E-07 4.9726 2.24157E-07 5.0600 1.28090E-07 5.0836 2.24157E-07 5.1190 1.92134E-07 5.1534 1.28090E-07 5.1839 1.60112E-07 5.2173 1.60112E-07 5.2683 1.12078E-06 5.2762 9.60672E-07 5.2880 9.60672E-07 5.3008 5.44381E-06 5.3126 4.16291E-06 5.3263 5.76403E-06 5.3401 4.80336E-06 5.3450 7.36516E-06
84-Po-210 2 ALPHAS REF B E,MEV. DK FRACTION 4.5168 1.07000E-05 5.3046 9.99989E-01	84-Po-211 3 ALPHAS REF B E,MEV. DK FRACTION 6.5694 5.40000E-03 6.8914 5.50000E-03 7.4502 9.89100E-01	86-Rn-220 2 ALPHAS REF A E,MEV. DK FRACTION 5.7490 7.00000E-04 6.2883 9.99300E-01	88-Ra-224 5 ALPHAS REF A E,MEV. DK FRACTION 5.0340 3.09945E-05 5.0470 7.19873E-05 5.1610 7.29872E-05 5.4490 4.89914E-02 5.6856 9.50833E-01	90-Th-227 19 ALPHAS REF B E,MEV. DK FRACTION 5.5862 1.81892E-03 5.6021 1.71707E-03 5.6136 2.22312E-03 5.6686 2.12207E-02 5.6940 1.51576E-02 5.7017 3.63783E-02 5.7097 8.28618E-02 5.7142 4.95150E-02 5.7572 2.02102E-01 5.7810 2.32417E-03 5.7952 1.13258E-03 5.8076 1.31366E-02 5.8667 2.42522E-02 5.9103 1.71787E-03 5.9166 7.88197E-03 5.9599 3.03153E-02 5.9779 2.32417E-01 6.0089 2.43048E-02 6.0383 2.42522E-01	91-Pa-231 19 ALPHAS REF A E,MEV. DK FRACTION 4.5090 3.02822E-05 4.5660 8.07526E-05 4.6000 1.51411E-04 4.6330 1.00941E-03 4.6440 1.00941E-03 4.6820 1.51411E-02 4.7130 1.00941E-02 4.7360 8.47902E-02 4.7960 4.03763E-04 4.8540 1.41317E-02 4.9020 2.01882E-05 4.9340 3.02822E-02 4.9517 2.30145E-01 4.9760 4.03763E-03 4.9860 1.41317E-02 5.0141 2.56390E-01 5.0297 2.01882E-01 5.0320 2.52352E-02 5.0590 1.11035E-01
83-Bi-211 2 ALPHAS REF B E,MEV. DK FRACTION 6.2790 1.59562E-01 6.6233 8.37698E-01	84-Po-211 3 ALPHAS REF B E,MEV. DK FRACTION 7.6285 5.00000E-04 8.0258 9.99500E-01	87-Fr-221 4 ALPHAS REF B E,MEV. DK FRACTION 6.0752 1.36426E-03 6.1275 1.37335E-01 6.2434 1.11236E-02 6.3411 8.49477E-01	89-Ac-225 13 ALPHAS REF B E,MEV. DK FRACTION 5.2871 2.30161E-03 5.4432 1.50105E-03 5.5520 1.00070E-03 5.5809 1.20084E-02 5.6093 1.20084E-02 5.6377 4.35305E-02 5.6824 1.25088E-02 5.7235 3.40238E-02 5.7320 1.01071E-01 5.7921 9.00630E-02 5.7939 1.80126E-01 5.8043 3.00210E-03 5.8299 5.06855E-01	90-Th-228 5 ALPHAS REF A E,MEV. DK FRACTION 5.1380 5.00050E-04 5.1770 1.80018E-03 5.2110 3.60036E-03 5.3405 2.67027E-01 5.4233 7.27073E-01	92-U-230 4 ALPHAS REF B E,MEV. DK FRACTION 5.6622 2.30023E-03 5.6661 3.60036E-03 5.8176 3.19032E-01 5.8886 6.75068E-01
84-Po-212 8 ALPHAS REF B E,MEV. DK FRACTION 5.3024 3.95857E-07 5.3456 3.59870E-06 5.4849 5.39805E-05 5.6069 3.95857E-03 5.6258 5.39805E-04 5.7684 6.00983E-03 6.0511 2.51549E-01 6.0902 9.78847E-02	84-Po-216 2 ALPHAS REF A E,MEV. DK FRACTION 5.9850 2.10000E-05 6.7785 9.99979E-01	87-Fr-222 1 ALPHA REF B E,MEV. DK FRACTION 5.7092 1.00000E-03	88-Ra-226 2 ALPHAS REF B E,MEV. DK FRACTION 4.6017 5.55000E-02 4.7846 9.44500E-01	90-Th-229 14 ALPHAS REF B E,MEV. DK FRACTION 4.7626 6.36107E-03 4.7987 1.28231E-02 4.8148 8.48142E-02 4.8390 4.84653E-02 4.8460 5.67447E-01 4.8622 1.81745E-03 4.9017 1.09047E-01 4.9309 1.11066E-03 4.9686 6.46204E-02 4.9795 3.23102E-02 5.0363 2.42326E-03 5.0492 5.25040E-02 5.0534 1.61551E-02 5.0783 1.00969E-04	91-Pa-231 19 ALPHAS REF A E,MEV. DK FRACTION 4.5090 3.02822E-05 4.5660 8.07526E-05 4.6000 1.51411E-04 4.6330 1.00941E-03 4.6440 1.00941E-03 4.6820 1.51411E-02 4.7130 1.00941E-02 4.7360 8.47902E-02 4.7960 4.03763E-04 4.8540 1.41317E-02 4.9020 2.01882E-05 4.9340 3.02822E-02 4.9517 2.30145E-01 4.9760 4.03763E-03 4.9860 1.41317E-02 5.0141 2.56390E-01 5.0297 2.01882E-01 5.0320 2.52352E-02 5.0590 1.11035E-01
84-Po-212 1 ALPHA REF B E,MEV. DK FRACTION 8.7846 1.00000E+00	84-Po-216 2 ALPHAS REF A E,MEV. DK FRACTION 6.4846 4.00100E-04 6.6113 1.00025E-04 6.8134 2.50063E-04 7.0677 9.99250E-01	87-Fr-222 1 ALPHA REF B E,MEV. DK FRACTION 5.7092 1.00000E-03	88-Ra-226 2 ALPHAS REF B E,MEV. DK FRACTION 4.6017 5.55000E-02 4.7846 9.44500E-01	90-Th-229 14 ALPHAS REF B E,MEV. DK FRACTION 4.7626 6.36107E-03 4.7987 1.28231E-02 4.8148 8.48142E-02 4.8390 4.84653E-02 4.8460 5.67447E-01 4.8622 1.81745E-03 4.9017 1.09047E-01 4.9309 1.11066E-03 4.9686 6.46204E-02 4.9795 3.23102E-02 5.0363 2.42326E-03 5.0492 5.25040E-02 5.0534 1.61551E-02 5.0783 1.00969E-04	91-Pa-231 19 ALPHAS REF A E,MEV. DK FRACTION 4.5090 3.02822E-05 4.5660 8.07526E-05 4.6000 1.51411E-04 4.6330 1.00941E-03 4.6440 1.00941E-03 4.6820 1.51411E-02 4.7130 1.00941E-02 4.7360 8.47902E-02 4.7960 4.03763E-04 4.8540 1.41317E-02 4.9020 2.01882E-05 4.9340 3.02822E-02 4.9517 2.30145E-01 4.9760 4.03763E-03 4.9860 1.41317E-02 5.0141 2.56390E-01 5.0297 2.01882E-01 5.0320 2.52352E-02 5.0590 1.11035E-01
83-Bi-213 2 ALPHAS REF B E,MEV. DK FRACTION 5.5508 1.62963E-03 5.8687 2.03704E-02	84-Po-218 2 ALPHAS REF B E,MEV. DK FRACTION 5.1810 1.10000E-05 6.0027 9.99989E-01	87-Fr-223 1 ALPHA REF B E,MEV. DK FRACTION 5.3330 4.00000E-05	88-Ra-226 2 ALPHAS REF B E,MEV. DK FRACTION 4.6017 5.55000E-02 4.7846 9.44500E-01	90-Th-229 14 ALPHAS REF B E,MEV. DK FRACTION 4.7626 6.36107E-03 4.7987 1.28231E-02 4.8148 8.48142E-02 4.8390 4.84653E-02 4.8460 5.67447E-01 4.8622 1.81745E-03 4.9017 1.09047E-01 4.9309 1.11066E-03 4.9686 6.46204E-02 4.9795 3.23102E-02 5.0363 2.42326E-03 5.0492 5.25040E-02 5.0534 1.61551E-02 5.0783 1.00969E-04	91-Pa-231 19 ALPHAS REF A E,MEV. DK FRACTION 4.5090 3.02822E-05 4.5660 8.07526E-05 4.6000 1.51411E-04 4.6330 1.00941E-03 4.6440 1.00941E-03 4.6820 1.51411E-02 4.7130 1.00941E-02 4.7360 8.47902E-02 4.7960 4.03763E-04 4.8540 1.41317E-02 4.9020 2.01882E-05 4.9340 3.02822E-02 4.9517 2.30145E-01 4.9760 4.03763E-03 4.9860 1.41317E-02 5.0141 2.56390E-01 5.0297 2.01882E-01 5.0320 2.52352E-02 5.0590 1.11035E-01
84-Po-213 2 ALPHAS REF B E,MEV. DK FRACTION 7.6123 3.00000E-05 8.3757 9.99970E-01	85-At-218 3 ALPHAS REF B E,MEV. DK FRACTION 6.6625 6.40000E-02 6.7045 9.00000E-01 6.7567 3.60000E-02	87-Fr-223 1 ALPHA REF B E,MEV. DK FRACTION 5.3330 4.00000E-05	88-Ra-226 2 ALPHAS REF B E,MEV. DK FRACTION 4.6017 5.55000E-02 4.7846 9.44500E-01	90-Th-229 14 ALPHAS REF B E,MEV. DK FRACTION 4.7626 6.36107E-03 4.7987 1.28231E-02 4.8148 8.48142E-02 4.8390 4.84653E-02 4.8460 5.67447E-01 4.8622 1.81745E-03 4.9017 1.09047E-01 4.9309 1.11066E-03 4.9686 6.46204E-02 4.9795 3.23102E-02 5.0363 2.42326E-03 5.0492 5.25040E-02 5.0534 1.61551E-02 5.0783 1.00969E-04	91-Pa-231 19 ALPHAS REF A E,MEV. DK FRACTION 4.5090 3.02822E-05 4.5660 8.07526E-05 4.6000 1.51411E-04 4.6330 1.00941E-03 4.6440 1.00941E-03 4.6820 1.51411E-02 4.7130 1.00941E-02 4.7360 8.47902E-02 4.7960 4.03763E-04 4.8540 1.41317E-02 4.9020 2.01882E-05 4.9340 3.02822E-02 4.9517 2.30145E-01 4.9760 4.03763E-03 4.9860 1.41317E-02 5.0141 2.56390E-01 5.0297 2.01882E-01 5.0320 2.52352E-02 5.0590 1.11035E-01

TABLE VII (cont.)

92- U-231 1 ALPHA REF B E,MEV. DK FRACTION 5.4539 5.50000E-05	92- U-235 12 ALPHAS REF A E,MEV. DK FRACTION N.1540 9.00000E-03 N.2170 5.70000E-02 N.2270 9.00000E-03 N.2710 4.00000E-03 N.3240 4.70000E-02 N.3640 1.70000E-01 N.3980 5.60000E-01 N.4160 2.10000E-02 N.4390 7.00000E-03 N.5020 1.70000E-02 N.5560 4.50000E-02 N.5980 5.40000E-02	93-NP-237 1 ALPHA REF A E,MEV. DK FRACTION N.5140 3.98843E-04 N.5810 3.98843E-03 N.5980 3.99017E-03 N.6391 6.16213E-02 N.6640 3.31040E-02 N.6940 4.78612E-03 N.7120 1.12673E-02 N.7659 7.97687E-02 N.7701 2.49277E-01 N.7882 4.68641E-01 N.8030 2.99133E-02 N.8170 2.49277E-02 N.8660 2.99133E-03 N.8730 2.59248E-02	94-PU-239 21 ALPHAS REF A E,MEV. DK FRACTION N.3990 2.50024E-07 N.5100 8.00078E-07 N.6300 7.00068E-06 N.6890 5.00048E-06 N.7360 4.50044E-05 N.7490 6.00058E-06 N.7690 8.00078E-06 N.7950 7.00068E-06 N.8280 2.40023E-05 N.8580 8.00078E-06 N.9110 2.00019E-06 N.9350 3.00029E-05 N.9620 3.00029E-05 N.9870 7.00068E-05 2.0080 8.00078E-05 2.0280 5.00048E-05 5.0540 2.10020E-04 5.0750 3.20031E-04 5.1046 1.15011E-01 5.1429 1.51015E-01 5.1554 7.33071E-01	95-AM-241 21 ALPHAS REF A E,MEV. DK FRACTION N.8000 9.00775E-07 N.8340 7.00063E-06 5.0040 1.00066E-06 5.0680 1.40121E-06 5.0890 4.00345E-06 5.0960 4.00345E-06 5.1140 4.00345E-06 5.1560 7.00063E-06 5.1780 3.00258E-06 5.1820 9.00775E-06 5.1940 6.00517E-06 5.2230 1.30112E-05 5.2440 2.40207E-05 5.2790 5.00431E-06 5.3220 1.50129E-04 5.3690 1.33115E-02 5.4170 1.00066E-04 5.4430 1.28110E-01 5.4857 6.52734E-01 5.5130 2.00172E-03 5.5443 3.50302E-03	96-CM-242 8 ALPHAS REF A E,MEV. DK FRACTION 5.1460 4.99796E-08 5.1840 2.49898E-07 5.5140 2.49898E-06 5.6090 1.99918E-07 5.8170 4.59812E-05 5.9720 3.59653E-04 6.0696 2.59844E-01 6.1129 7.39697E-01	95-AM-243 13 ALPHAS REF A E,MEV. DK FRACTION 4.6950 1.60296E-05 4.9190 8.51572E-07 4.9300 1.80335E-06 4.9460 3.40629E-06 5.0080 1.60296E-05 5.0320 6.20407E-05 5.0860 4.00740E-05 5.1130 5.40949E-05 5.1810 1.10203E-02 5.2335 1.10203E-01 5.2754 8.75616E-01 5.3210 1.20222E-03 5.3492 1.80333E-03	96-CM-243 28 ALPHAS REF A E,MEV. DK FRACTION 5.2260 3.86407E-06 5.2600 1.46041E-06 5.3150 9.90940E-06 5.3220 2.97282E-05 5.3310 2.97282E-05 5.5220 1.98188E-05 5.5310 5.94564E-05 5.5360 1.98188E-05 5.5670 6.93658E-05 5.5740 6.93658E-05 5.5810 8.91846E-05 5.5860 1.98188E-04 5.5920 4.90940E-05 5.6080 9.90940E-05 5.6110 3.96376E-04 5.6210 5.94564E-04 5.6380 1.38732E-03 5.6450 2.97282E-04 5.6810 1.98188E-04 5.6850 1.58550E-02 5.7415 1.13956E-01 5.7847 7.25368E-01 5.8750 6.93658E-03 5.9060 9.90940E-04 5.9920 5.64836E-02 6.0090 1.09003E-02 6.0560 4.65742E-02 6.0670 1.46641E-02						
92- U-232 7 ALPHAS REF A E,MEV. DK FRACTION N.5090 2.39800E-07 N.9291 2.09625E-06 N.9460 1.69859E-06 N.9973 2.89759E-05 5.1373 2.79767E-03 5.2635 3.11740E-01 5.3203 6.85429E-01	93-NP-235 11 ALPHAS REF B E,MEV. DK FRACTION N.8042 1.60160E-08 N.8599 1.12112E-07 N.9227 1.84184E-06 N.9365 9.60961E-08 N.9393 9.60961E-07 5.0024 8.60961E-08 5.0033 8.00801E-07 5.0203 8.48849E-06 5.0455 2.88288E-07 5.0940 3.20320E-08 5.1030 2.40240E-07	94-PU-237 2 ALPHAS REF A E,MEV. DK FRACTION 5.3600 2.60700E-05 5.6500 6.93000E-06	94-PU-240 5 ALPHAS REF A E,MEV. DK FRACTION N.4800 2.10015E-07 N.8510 2.00014E-05 5.0140 9.10064E-04 5.1234 2.65018E-01 5.1683 7.34051E-01	96-CM-241 11 ALPHAS REF A E,MEV. DK FRACTION 5.6870 2.20044E-05 5.7190 8.00160E-06 5.7850 7.00140E-06 5.8630 1.40028E-05 5.8843 1.18024E-03 5.9140 1.20024E-05 5.9260 1.81036E-03 5.9386 6.89138E-03 5.9780 2.80056E-05 6.0360 1.20024E-05 6.0820 1.50030E-05	94-PU-242 4 ALPHAS REF A E,MEV. DK FRACTION N.5985 1.30001E-05 N.7546 9.80007E-04 N.8563 2.24002E-01 N.9006 7.75005E-01	95-AM-242M 7 ALPHAS REF A E,MEV. DK FRACTION 5.0650 1.20056E-05 5.0860 1.53672E-05 5.1400 2.90537E-04 5.2050 4.27401E-03 5.3130 3.84181E-05 5.3650 7.20339E-05 5.4080 5.76271E-05	94-PU-241 11 ALPHAS REF A E,MEV. DK FRACTION N.6920 7.35662E-09 N.7320 7.35662E-09 N.7420 1.71654E-08 N.7830 4.90441E-08 N.7970 2.94265E-07 N.8535 2.96717E-06 N.8965 2.04024E-05 N.9720 3.18787E-07 N.9990 1.00540E-07 5.0420 2.50125E-07 5.0540 8.58272E-08	92- U-238 3 ALPHAS REF A E,MEV. DK FRACTION N.0390 2.29472E-03 N.1490 2.29472E-01 N.1960 7.68233E-01	94-PU-238 11 ALPHAS REF A E,MEV. DK FRACTION N.5670 1.10071E-09 N.5880 1.60104E-08 N.6620 3.00195E-08 N.6640 3.00195E-09 N.7030 9.00584E-07 N.7260 1.00065E-07 5.0110 7.00455E-08 5.2080 5.00325E-05 5.3590 1.30084E-03 5.4565 2.87186E-01 5.4992 7.11462E-01	94-PU-235 1 ALPHA REF B E,MEV. DK FRACTION 5.8556 1.30000E-04	92- U-236 3 ALPHAS REF A E,MEV. DK FRACTION N.3310 2.59326E-03 N.4450 2.59326E-01 N.4940 7.38081E-01	94-PU-236 6 ALPHAS REF A E,MEV. DK FRACTION 5.0880 6.00103E-06 5.2140 2.70046E-06 5.4520 2.00034E-05 5.6150 1.80031E-03 5.7210 3.09053E-01 5.7680 6.89118E-01	92- U-234 5 ALPHAS REF A E,MEV. DK FRACTION N.1200 3.29013E-07 N.2740 4.48654E-07 N.6030 2.99102E-03 N.7228 2.74177E-01 N.7730 7.22831E-01

TABLE VII (cont.)

94-PU-244		97-BK-249		98-CF-252		99-ES-254	
2 ALPHAS, REF A		7 ALPHAS, REF A		5 ALPHAS, REF A		8 ALPHAS, REF B	
E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION
4.5460	1.93757E-01	5.0450	1.45291E-08	5.6160	5.80623E-07	6.2669	2.21953E-03
4.5890	8.04993E-01	5.1150	3.92285E-07	5.8263	1.93541E-05	6.2758	1.61421E-03
96-CM-244		98-CF-249		98-CF-253		99-ES-254M	
8 ALPHAS, REF A		16 ALPHAS, REF A		2 ALPHAS, REF A		7 ALPHAS, REF B	
E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION
4.9200	8.99767E-07	5.3510	1.99410E-05	5.9210	1.64300E-04	6.2472	7.37056E-05
4.9600	1.99948E-06	5.4310	9.97049E-05	5.9790	2.93570E-03	6.2797	2.78071E-04
5.2150	1.19969E-06	5.5020	4.38701E-04	99-ES-253		6.3045	2.51269E-03
5.3130	3.99896E-07	5.5590	1.09675E-03	28 ALPHAS, REF A		6.3405	6.03046E-05
5.5130	3.49909E-05	5.6230	1.99410E-04	E,MEV.	DK FRACTION	6.4361	4.69036E-05
5.6640	2.19943E-04	5.6940	2.99115E-03	5.7300	8.00043E-07	6.4791	1.94315E-04
5.7628	2.35939E-01	5.7597	4.78583E-02	5.9100	2.70015E-07	6.5130	1.34010E-04
5.8050	7.63802E-01	5.7840	2.49262E-03	5.9350	4.00022E-07	100-FM-254	
96-CM-245		98-CF-250		98-CF-251		3 ALPHAS, REF B	
6 ALPHAS, REF A		4 ALPHAS, REF A		14 ALPHAS, REF A		E,MEV.	DK FRACTION
E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	7.0492	9.00369E-03
5.2346	3.20256E-03	5.8120	8.23562E-01	5.7367	9.99130E-05	7.1468	1.40057E-01
5.3038	4.97398E-02	5.8495	1.39587E-02	5.8900	2.99739E-03	7.1889	8.50349E-01
5.3620	9.32546E-01	5.9034	3.19056E-02	5.9891	1.61859E-01	99-ES-255	
5.4363	4.00320E-04	5.9462	3.38997E-02	6.0308	8.34274E-01	3 ALPHAS, REF B	
5.4887	8.30665E-03	6.0000	5.98229E-04	98-CF-254		E,MEV.	DK FRACTION
5.5292	5.80464E-03	6.0720	3.98819E-03	2 ALPHAS, REF B		5.7943	5.27000E-04
96-CM-246		98-CF-251		98-CF-254		100-FM-254	
2 ALPHAS, REF A		4 ALPHAS, REF A		2 ALPHAS, REF B		1 ALPHA, REF B	
E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION
5.3430	2.09945E-01	5.7367	9.99130E-05	5.8366	2.57300E-03	6.9152	1.00000E+00
5.3860	7.89793E-01	5.8900	2.99739E-03	100-FM-255		5 ALPHAS, REF B	
96-CM-247		98-CF-251		98-CF-254		E,MEV. DK FRACTION	
7 ALPHAS, REF A		14 ALPHAS, REF A		2 ALPHAS, REF B		6.8069	1.10375E-03
E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	6.8915	6.22115E-03
4.8140	4.70000E-02	5.5010	3.04569E-03	5.8366	2.57300E-03	6.9634	5.01706E-02
4.8680	7.10000E-01	5.5660	1.52284E-02	100-FM-256		6.9829	1.30444E-03
4.9410	1.60000E-02	5.6030	2.03046E-03	1 ALPHA, REF B		7.0225	9.37186E-01
4.9830	2.00000E-02	5.6320	4.56853E-02	E,MEV.	DK FRACTION	7.0800	4.01365E-03
5.1450	1.20000E-02	5.6480	3.55330E-02	100-FM-257		5 ALPHAS, REF B	
5.2100	5.70000E-02	5.6770	3.53299E-01	5 ALPHAS, REF B		E,MEV.	DK FRACTION
5.2650	1.38000E-01	5.7380	1.01523E-02	5.8366	2.57300E-03	6.3467	3.01811E-03
96-CM-248		98-CF-251		98-CF-254		6.4410	
2 ALPHAS, REF A		14 ALPHAS, REF A		2 ALPHAS, REF B		2.01207E-02	
E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	6.5199	9.35614E-01
5.0340	1.66049E-01	5.7620	3.85787E-02	100-FM-257		6.6965	3.52113E-02
5.0780	7.51351E-01	5.7930	2.03046E-02	5 ALPHAS, REF B		6.7572	6.03622E-03
98-CF-248		98-CF-251		98-CF-254		E,MEV. DK FRACTION	
2 ALPHAS, REF B		14 ALPHAS, REF A		2 ALPHAS, REF B		3.01811E-03	
E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	E,MEV.	DK FRACTION	2.01207E-02	
6.2241	1.80000E-01	5.8140	4.26396E-02	100-FM-257		9.35614E-01	
6.2663	8.20000E-01	5.8520	2.78173E-01	5 ALPHAS, REF B		3.52113E-02	
		5.9430	6.09137E-03	E,MEV.	DK FRACTION	6.03622E-03	
		6.0140	1.21827E-01				
		6.0740	2.74112E-02				

REFERENCE A= ENDFB/B-V
 REFERENCE B= TABLE OF ISOTOPES, SEVENTH EDITION

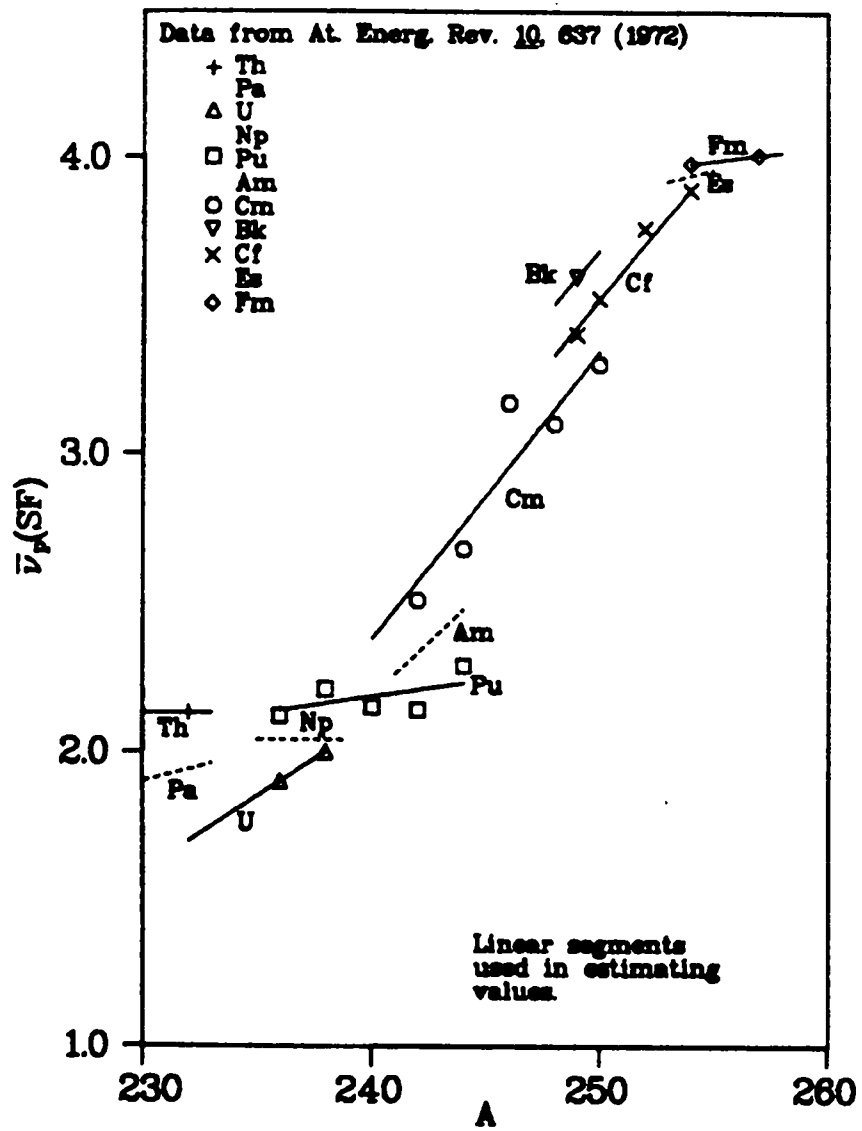


Fig. 4.
Values of $\bar{\nu}_p(\text{SF})$.

TABLE VIII

SPONTANEOUS-FISSION NEUTRON PRODUCTION BY ACTINIDE DECAY

NUCLIDE	NU-BAR VALUES			SPONTANEOUS FISSION BRANCHING	NEUTRONS PER NUCLIDE DECAY
	PROMPT	DELAYED	TOTAL		
90-TH-230	2.13	.01	2.14	5.330-13 A	1.14 -12
91-PA-231	1.92	.01	1.93	2.980-12 A	5.75 -12
90-TH-232	2.130+.200 B	.01	2.14	1.410-11 A	3.02 -11
92- U-232	1.70	.01	1.71	9.000-13 C	1.54 -12
92- U-233	1.75	.01	1.76	1.300-12 C	2.29 -12
92- U-234	1.80	.01	1.81	1.200-11 C	2.17 -11
92- U-235	1.85	.01	1.86	2.011-09 A	3.74 -09
92- U-236	1.900+.050 B	.01	1.91	1.200-09 C	2.29 -09
94-PU-236	2.120+.130 B	.01	2.13	8.100-10 C	1.73 -09
93-NP-237	2.04	.01	2.05	2.140-12 A	4.39 -12
92- U-238	2.000+.030 B	.01	2.01	5.450-07 C	1.095-06
94-PU-238	2.210+.130 B	.01	2.22	1.840-09 C	4.08 -09
94-PU-239	2.15	.01	2.16	4.400-12 C	9.37 -12
94-PU-240	2.151+.006 B	.01	2.16	5.000-08 C	1.08 -07
96-CM-240	2.38	.01	2.39	3.860-08 A	9.23 -08
95-AM-241	2.26	.01	2.27	4.100-12 C	9.31 -12
94-PU-242	2.141+.190 B	.01	2.15	5.500-06 C	1.18 -05
95-AM-242M	2.33	.01	2.34	1.600-10 C	3.74 -10
96-CM-242	2.510+.060 B	.01	2.52	6.800-08 C	1.71 -07
95-AM-243	2.41	.01	2.42	2.200-10 C	5.32 -10
94-PU-244	2.290+.190 B	.01	2.30	1.250-03 C	2.88 -03
96-CM-244	2.681+.011 B	.01	2.69	1.347-06 C	3.62 -06
96-CM-246	3.170+.220 B	.01	3.18	2.614-04 C	8.31 -04
96-CM-248	3.100+.090 B	.01	3.11	8.260-02 C	2.569-01
98-CF-248	3.33	.01	3.34	2.850-05 A	9.52 -05
97-Bk-249	3.590+.160 B	.01	3.60	4.600-10 C	1.66 -09
98-CF-249	3.400+.400 B	.01	3.41	5.020-09 A	1.71 -08
96-CM-250	3.300+.080 B	.01	3.31	7.000-01 D	2.32 +00
98-CF-250	3.520+.090 B	.01	3.53	3.092-02 C	2.72 -03
98-CF-252	3.756+.012 B	.009 B	3.765+.010 B	3.092-02 C	1.164-01
99-ES-253	3.92	.01	3.93	8.700-08 C	3.42 -07
98-CF-254	3.890+.050 B	.01	3.890+.050 E	9.969-01 A	3.88 +00
99-ES-254	3.94	.01	3.95	3.020-08 A	1.19 -07
99-ES-254M	3.94	.01	3.95	4.500-08 A	1.78 -07
100-FM-254	3.980+.140 B	.01	3.96 +.14 F	5.900-04 A	2.34 -03
99-ES-255	3.96	.01	3.97	4.000-05 A	1.59 -04
100-FM-255	3.99	.01	3.73 +.18 F	2.290-07 A	8.54 -07
100-FM-256	4.00	.01	4.01	9.190-01 A	3.69 +00
100-FM-257	4.010+.130 B	.01	3.85 +.05 G	2.100-03 A	8.09 -03
100-FM-258	4.02	.01	4.03	1.000+00 A	4.03 +00

DATA REFERENCES USED

A=TABLE OF ISOTOPIES, SEVENTH EDITION

B=MANERO AND KONSHIN, ATOMIC ENERGY REV. 10,637-756(1972)

C=ENDF/B-V

D=A. TOBIAS, U.K., PRIVATE COMMUNICATION

E=C. J. ORTH, NUCL. SCI. ENG. 43, 54 (1971)

F=Y. A. LAZAREV, ATOMIC ENERGY REV. 15, 75 (1977)

G=D. C. HOFFMAN ET AL., PHYS. REV. C21, 637 (1980)

ADDITIONAL REFERENCES SURVEYED

J. U. BOLDREMAN, IN NEUTRON STD. REF. DATA, I.A.E.A. VIENNA (1974)

J. P. BALAGNA ET AL., PHYS. REV. LETT. 26, 145 (1971)

PROMPT NU-BAR VALUES GIVEN WITHOUT REFERENCE HAVE BEEN ESTIMATED FROM THE VALUES OF REFERENCE B. DELAYED NU-BAR VALUES GIVEN WITHOUT REFERENCE HAVE BEEN ARBITRARILY ASSUMED.

IV. CALCULATION OF THE THICK-TARGET NEUTRON-PRODUCTION FUNCTION $P_i(E_\alpha)$

The neutron-production function $P_i(E_\alpha)$ defined by Eqs. (6) and (9) gives the contribution from reactions with nuclide i to the probability of neutron production by a decay alpha particle of energy E_α emitted within the material. The POFEAL code calculates values of P_i OF E -ALPHA using the algorithm

$$P(J) = 1.E + 6* \frac{N_i}{N} \sum_{j=2}^J \frac{[\sigma_i(j-1) + \sigma_i(j)]/2}{[\epsilon(j-1) + \epsilon(j)]/2} [E(j) - E(j-1)] \quad , \quad (25)$$

where

N_i is the atom density of nuclide i (atoms/cm³),

N is the total atom density (atoms/cm³),

E_j is the j th regular energy point at or above the cross-section threshold (MeV),

$\sigma_i(j)$ is the value of the (α, n) cross section of nuclide i at E_j (mb),

$\epsilon(j)$ is the value of the stopping cross section (eV/10¹⁵ atoms/cm²),

and the leading quantity of 1×10^6 is required because of the units of σ , ϵ , and E .

The ¹⁷O and ¹⁸O contributions to the (α, n) neutron-production rate are given in Tables IX-XII for each of the four fuel compositions given in Table I. Values for the four compositions at any energy differ by less than 4%. The ¹⁷O and ¹⁸O contributions to (α, n) neutron production in spent UO₂ fuel are shown in Fig. 5.

V. RESULTS

The half-lives, average decay energies, and spent UO₂ fuel neutron-production values $R_k(\alpha, n)$, $R_k(\text{SF})$, and R_k for each of the actinide nuclides k are given in Table XIII. Values of $R_k(\text{SF})$ are repeated from Table VIII. Values of $R_k(\alpha, n)$ were obtained using the alpha spectra data of Table VII and $P(E_\alpha)$ values given in Table XI for ^{17,18}O(α, n) in spent UO₂ fuel.

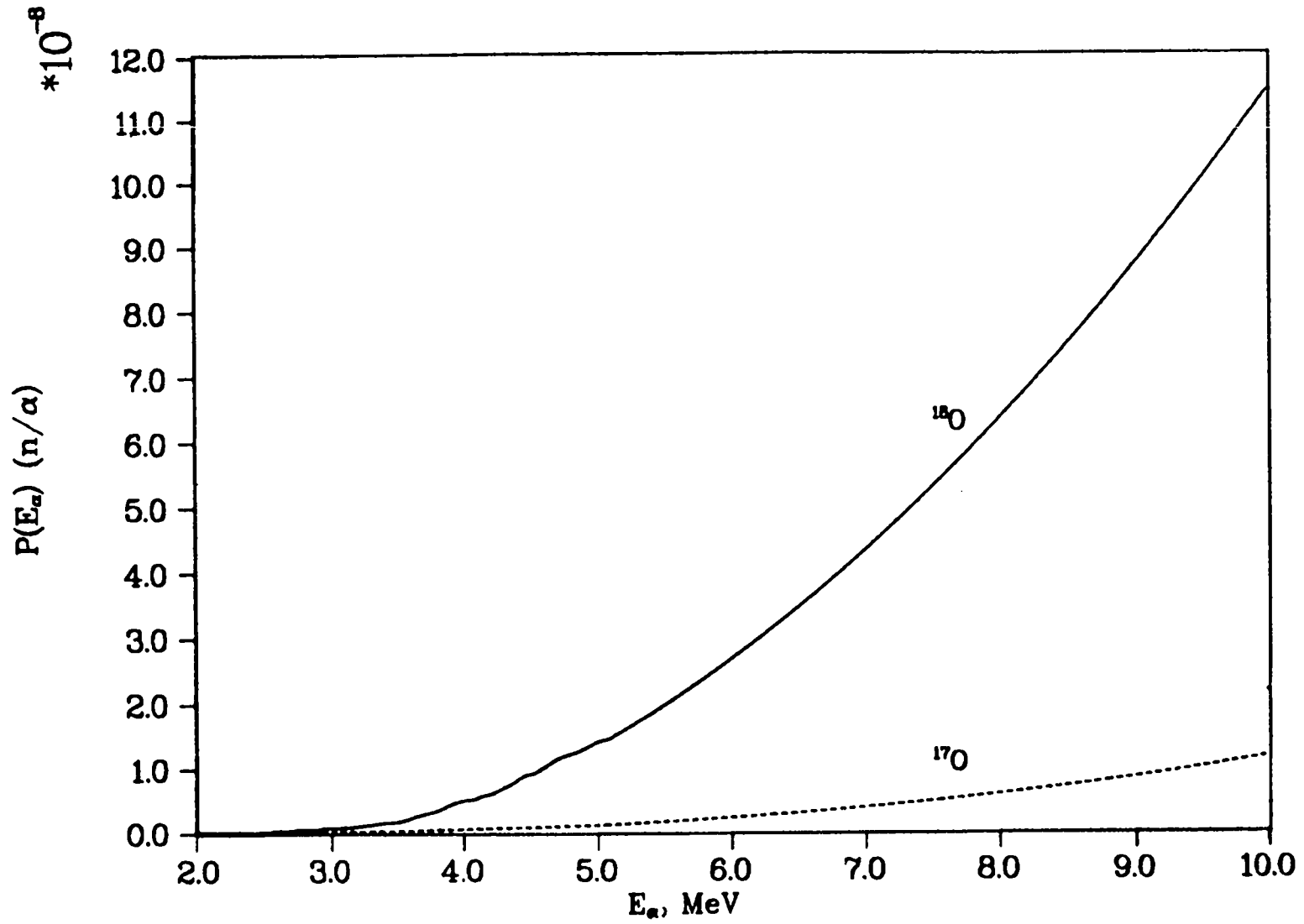


Fig. 5.
 $^{17,18}\text{O}(\alpha,n)$ neutron production by decay alphas in LWR irradiated UO_2 fuel.

TABLE XIII

NEUTRON PRODUCTION FROM ACTINIDE DECAY IN UO₂ FUEL

NUCLIDE	HALF-LIFE (SECONDS)	DECAY ENERGY (MEV)	DE- CAY REF	◆◆◆◆NEUTRONS PER DECAY◆◆◆◆		
				ALPHA,N IN UO ₂	SPONT. FISSION	TOTAL
80-HG-206	4.89000+2	0.5274	A	0.	0.	0.
81-TL-206	2.50980+2	0.5402	A	0.	0.	0.
82-PB-206	STABLE	0.	-	0.	0.	0.
81-TL-207	2.87400+2	0.5194	A	0.	0.	0.
82-PB-207	STABLE	0.	-	0.	0.	0.
81-TL-208	1.84200+2	3.9702	B	0.	0.	0.
82-PB-208	STABLE	0.	-	0.	0.	0.
81-TL-209	1.32000+2	2.8315	A	0.	0.	0.
82-PB-209	1.17108+4	0.2234	A	0.	0.	0.
83-BI-209	6.3115+25	0.	A	0.	0.	0.
81-TL-210	7.80000+1	4.2765	A	0.	0.	7.00 -05
82-PB-210	7.02472+8	0.0441	A	5.68 -17	0.	5.68 -17
83-BI-210	4.33123+5	0.3899	A	1.56 -14	0.	1.16 -14
84-PO-210	1.19557+7	5.4076	A	1.87 -08	0.	1.87 -08
82-PB-211	2.16600+3	0.5353	A	0.	0.	0.
83-BI-211	1.29000+2	6.7881	A	3.88 -08	0.	3.88 -08
84-PO-211	0.5160000	7.5942	A	5.64 -08	0.	5.64 -08
82-PB-212	3.83040+4	0.3180	B	0.	0.	0.
83-BI-212	3.63600+3	2.9030	A	1.076 -08	0.	1.076 -08
84-PO-212	2.96000-7	8.9536	A	8.94 -08	0.	8.94 -08
83-BI-213	2.73540+3	0.7172	A	5.85 -10	0.	5.85 -10
84-PO-213	4.20000-6	8.5360	A	7.86 -08	0.	7.86 -08
82-PB-214	1.60800+3	0.5389	A	0.	0.	0.
83-BI-214	1.18200+3	2.1923	A	4.39 -12	0.	4.39 -12
84-PO-214	1.63700-4	7.8337	A	6.19 -08	0.	6.19 -08
83-BI-215	4.44000+2	0.8445	A	0.	0.	0.
84-PO-215	1.77800-3	7.5265	A	5.52 -08	0.	5.52 -08
85-AT-215	1.00000-4	8.1780	A	6.98 -08	0.	6.98 -08
84-PO-216	0.1500000	6.9064	B	4.28 -08	0.	4.28 -08
85-AT-217	0.0323000	7.2004	A	4.85 -08	0.	4.85 -08
86-RN-217	5.40000-4	7.8880	A	6.32 -08	0.	6.32 -08
84-PO-218	1.83000+2	6.1149	A	2.909 -08	0.	2.909 -08
85-AT-218	1.7500000	6.8830	A	4.14 -08	0.	4.14 -08
86-RN-218	0.0350000	7.2664	A	4.99 -08	0.	4.99 -08
85-AT-219	5.40000+1	6.2165	A	3.26 -08	0.	3.26 -08
86-RN-219	3.9600000	6.9463	A	4.25 -08	0.	4.25 -08
86-RN-220	5.56000+1	6.4048	B	3.39 -08	0.	3.39 -08
87-FR-221	2.88000+2	6.4580	A	3.45 -08	0.	3.45 -08
86-RN-222	3.30351+5	5.5905	A	2.129 -08	0.	2.129 -08
87-FR-222	8.64000+2	0.7450	A	2.45 -11	0.	2.45 -11
88-RA-222	3.80000+1	6.6760	A	3.846 -08	0.	3.846 -08
87-FR-223	1.30800+3	0.4559	A	7.65 -13	0.	7.65 -13
88-RA-223	9.87949+5	-----	A	2.39 -08	0.	2.39 -08
88-RA-224	3.16224+5	5.7903	B	2.40 -08	0.	2.40 -08
88-RA-225	1.27872+6	0.1433	A	0.	0.	0.
89-AC-225	8.64000+5	5.9354	A	2.57 -08	0.	2.57 -08
88-RA-226	5.0461+10	4.8708	A	1.304 -08	0.	1.304 -08
89-AC-226	1.04400+5	0.4099	A	1.24 -12	0.	1.24 -12

TABLE XIII (cont.)

NUCLIDE	HALF-LIFE (SECONDS)	DECAY ENERGY (MEV)	DE- CAY REF	◆◆◆◆NEUTRONS PER DECAY◆◆◆◆					
				ALPHA	N FISSION	SPONT. TOTAL			
90-TH-226	1.85400+3	6.4517	A	3.42	-08	0.	3.42	-08	
89-AC-227	6.87097+8	0.0878	A	2.01	-10	0.	2.01	-10	
90-TH-227	1.61720+6	6.1466	A	2.72	-08	0.	2.72	-08	
88-PA-228	1.82087+8	0.0146	A	0.		0.	0.		
89-AC-228	2.20680+4	1.3696	A	0.		0.	0.		
90-TH-228	6.03725+7	5.5176	B	2.004	-08	0.	2.004	-08	
90-TH-229	2.3163+11	5.1686	A	1.391	-08	0.	1.391	-08	
90-TH-230	2.4299+12	4.7609	B	1.207	-08	1.14	-12	1.21	-08
91-PA-230	1.52928+6	0.6577	A	6.03	-13	0.	6.03	-13	
92- U-230	1.79712+6	5.9928	A	2.69	-08	0.	2.69	-08	
90-TH-231	9.18720+4	0.1537	B	0.		0.	0.		
91-PA-231	1.0338+12	5.0601	B	1.478	-08	5.75	-12	1.48	-08
92- U-231	3.62880+5	0.1017	A	1.14	-12	0.	1.14	-12	
90-TH-232	4.4337+17	4.0882	B	5.52	-09	3.02	-11	5.55	-09
91-PA-232	1.13184+5	1.098	B	0.		0.	0.		
92- U-232	2.26263+9	5.4145	B	1.871	-08	1.54	-12	1.87	-08
90-TH-233	1.33800+3	0.4422	B	0.		0.	0.		
91-PA-233	2.33280+6	0.4080	B	0.		0.	0.		
92- U-233	5.0232+12	4.8978	B	1.336	-08	2.29	-12	1.34	-08
90-TH-234	2.08233+6	0.1473	A	0.		0.	0.		
91-PA-234	2.43000+4	2.2453	A	0.		0.	0.		
91-PA-234M	7.05000+1	0.8141	A	0.		0.	0.		
92- U-234	7.7188+12	4.8685	B	1.299	-08	2.17	-11	1.301	-08
90-TH-235	4.14000+2	-----	A	0.		0.	0.		
91-PA-235	1.45200+3	-----	A	0.		0.	0.		
92- U-235	2.2210+16	4.6651	B	8.89	-09	3.74	-09	1.26	-08
92- U-235M	1.48080+3	0.0001	A	0.		0.	0.		
93-NP-235	3.42230+7	0.0810	A	2.44	-13	0.	2.44	-13	
94-PU-235	1.53600+3	5.8675	A	3.48	-12	0.	3.48	-12	
92- U-236	7.3890+14	4.5809	B	9.89	-09	2.29	-09	1.218	-08
93-NP-236	3.6290+12	0.3390	B	0.		0.	0.		
93-NP-236M	8.10000+4	0.1353	B	0.		0.	0.		
94-PU-236	8.99688+7	5.8634	B	2.517	-08	1.73	-09	2.69	-08
92- U-237	5.83200+5	0.3103	B	0.		0.	0.		
93-NP-237	6.7532+13	4.9470	B	1.303	-08	4.39	-12	1.303	-08
94-PU-237	3.94243+6	0.0628	B	6.72	-13	0.	6.72	-13	
92- U-238	1.4100+17	4.2755	B	6.64	-09	1.095	-06	1.102	-06
93-NP-238	1.82908+5	0.7916	B	0.		0.	0.		
94-PU-238	2.76912+9	5.5871	B	2.124	-08	4.08	-09	2.532	-08
92- U-239	1.41000+3	0.4650	B	0.		0.	0.		
93-NP-239	2.03385+5	0.4180	B	0.		0.	0.		
94-PU-239	7.6084+11	5.2396	B	1.664	-08	9.37	-12	1.665	-08
92- U-240	5.07600+4	0.1755	A	0.		0.	0.		
93-NP-240	4.02000+3	1.5755	A	0.		0.	0.		
93-NP-240M	4.50000+2	1.0407	A	0.		0.	0.		
94-PU-240	2.0670+11	5.3274	B	1.676	-08	1.08	-07	1.25	-07
95-AM-240	1.82880+5	1.0920	B	3.74	-14	0.	3.74	-14	
96-CM-240	2.31552+6	6.3844	A	3.37	-08	9.23	-08	1.26	-07
94-PU-241	4.63886+8	0.0054	B	3.39	-13	0.	3.39	-13	
95-AM-241	1.3639+10	5.6131	B	2.115	-08	9.31	-12	2.116	-08
96-CM-241	2.83392+6	1.1100	B	2.79	-10	0.	2.79	-10	
94-PU-242	1.1875+13	4.9812	B	1.406	-08	1.18	-05	1.18	-05
95-AM-242	5.76360+4	0.1944	B	0.		0.	0.		
95-AM-242M	4.79665+9	0.0631	B	9.22	-11	3.74	-10	4.56	-10

TABLE XIII (cont.)

NUCLIDE	HALF-LIFE (SECONDS)	DECAY ENERGY (MEV)	DE- CAY REF	◆◆◆◆NEUTRONS PER DECAY◆◆◆◆		
				ALPHA, IN UO ₂	N FISSION	SPONT. FISSION
96-CM-242	1.40745+7	6.2169	B	3.07 -08	1.714-07	2.02 -07
94-FU-243	1.78452+4	0.1957	B	0.	0.	0.
95-AM-243	2.3289+11	5.4224	B	1.82 -08	5.32 -10	1.87 -08
96-CM-243	8.99372+8	6.1598	B	2.62 -08	0.	2.62 -08
94-FU-244	2.5877+15	4.6510	B	1.083-08	2.875-03	2.88 -03
95-AM-244	3.63600+4	1.1177	B	0.	0.	0.
95-AM-244M	1.56000+3	0.5088	B	0.	0.	0.
96-CM-244	5.71495+8	5.9010	B	2.582-08	3.623-06	3.65 -06
94-FU-245	3.78280+4	0.8103	A	0.	0.	0.
95-AM-245	7.38000+3	0.3199	A	0.	0.	0.
96-CM-245	2.6744+11	5.5881	B	1.948-08	0.	1.95 -08
94-FU-246	9.37440+5	0.2514	A	0.	0.	0.
95-AM-246M	1.50000+3	1.4433	A	0.	0.	0.
96-CM-246	1.4926+11	5.4714	B	1.971-08	8.313-04	8.31 -04
96-CM-247	4.9229+14	5.3522	B	1.466-08	0.	1.47 -08
96-CM-248	1.0720+13	4.7270	B	1.441-08	2.569-01	2.57 -01
97-BK-248	2.84018+8	-----	A	-----	-----	-----
97-BK-248M	8.46000+4	0.1684	A	0.	0.	0.
98-CF-248	2.88144+7	6.3613	A	3.336-08	9.519-05	9.52 -05
96-CM-249	3.84900+3	0.2932	B	0.	0.	0.
97-BK-249	2.76480+7	0.0331	B	2.906-13	1.656-09	1.66 -09
98-CF-249	1.1064+10	6.2903	B	2.646-08	1.712-08	4.36 -08
96-CM-250	3.5660+11	-----	C	-----	2.32 +00	2.32 +00
97-BK-250	1.15812+4	1.1829	B	0.	0.	0.
98-CF-250	4.12764+8	6.1227	B	2.941-08	2.718-03	2.72 -03
96-CM-251	1.00800+3	0.5925	A	0.	0.	0.
97-BK-251	3.33600+3	0.4988	A	0.	0.	0.
98-CF-251	2.8338+10	6.0260	B	2.532-08	0.	2.53 -08
98-CF-252	8.32471+7	6.0317	B	2.996-08	1.164-01	1.164-01
98-CF-253	1.53878+6	0.0980	B	8.89 -11	0.	8.89 -11
99-ES-253	1.76860+6	6.7367	B	3.995-08	3.419-07	3.82 -07
98-CF-254	5.22720+6	0.0184	A	8.167-11	3.88 +00	3.88 +00
99-ES-254	2.38205+7	6.6172	A	3.627-08	1.193-07	1.56 -07
99-ES-254M	1.41480+5	0.7351	A	1.138-10	1.778-07	1.78 -07
100-FM-254	1.16640+4	7.2996	A	5.08 -08	2.34 -03	2.34 -03
98-CF-255	6.84000+3	-----	A	0.	0.	0.
99-ES-255	3.30912+6	0.5956	A	2.72 -09	1.59 -04	1.59 -04
100-FM-255	7.22520+4	7.2407	A	4.75 -08	8.54 -07	9.02 -07
99-ES-256	1.32000+3	0.6169	A	0.	0.	0.
100-FM-256	9.45720+3	7.0250	A	4.55 -08	3.69 +00	3.69 +00
100-FM-257	8.68320+6	6.8640	A	3.81 -08	8.09 -03	8.09 -03
100-FM-258	3.80000-4	-----	A	0.	4.03 +00	4.03 +00

DECAY DATA REFERENCES

A=TABLE OF ISOTOPIES

B=ENDF/B-V

C=A.TOBIAS,U.K.,PRIVATE COMMUNICATION

ADDITIONAL NOTES

MISSING DATA NOTED AS -----

81-TL-210, NEUTRONS FROM DELAYED NEUTRON
EMISSION FROM 82-PB-210 LEVELS
PRODUCED IN BETA DECAY.92- U-235, SPONTANEOUS FISSION BRANCHING
IN ENDF/B-V IS ZERO BY OMISSION.
S.F. BRANCHING(2.011-9) TAKEN
FROM REFERENCE A.

97-BK-248 DECAY CHARACTERISTICS UNKNOWN.

These values of R_k may be used with detailed calculated activity inventory to determine total neutron production within oxide fuel, using Eq. (22).

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